

Medical Robotics Group Coursework

Group 14:

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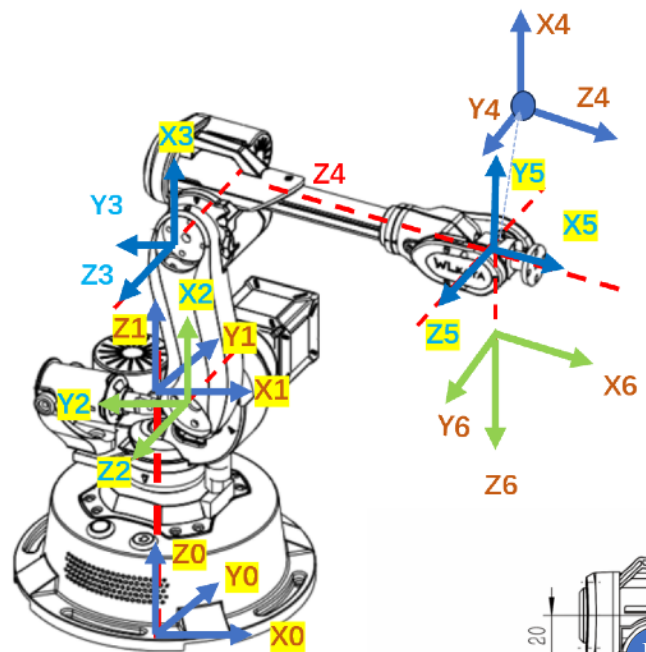
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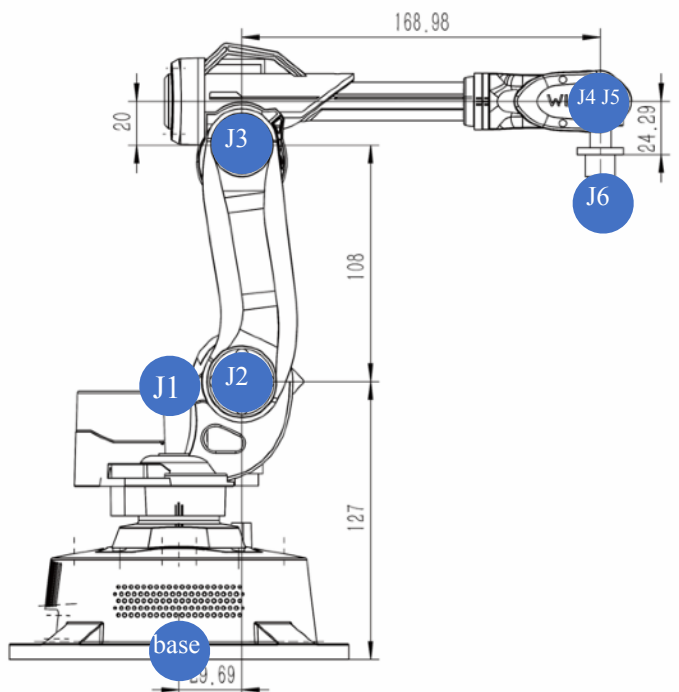


Task 1

Robot Modelling and MDH Table



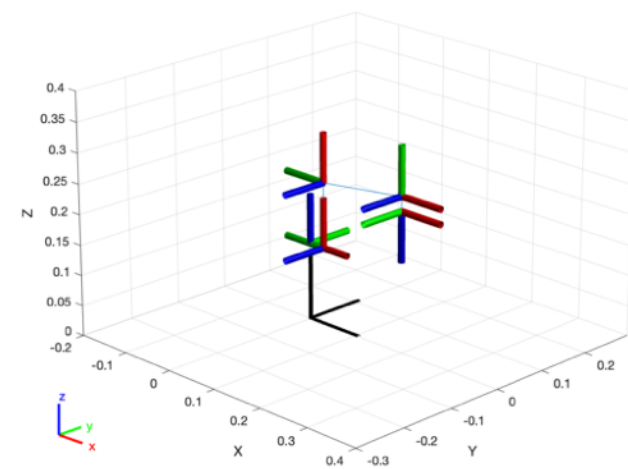
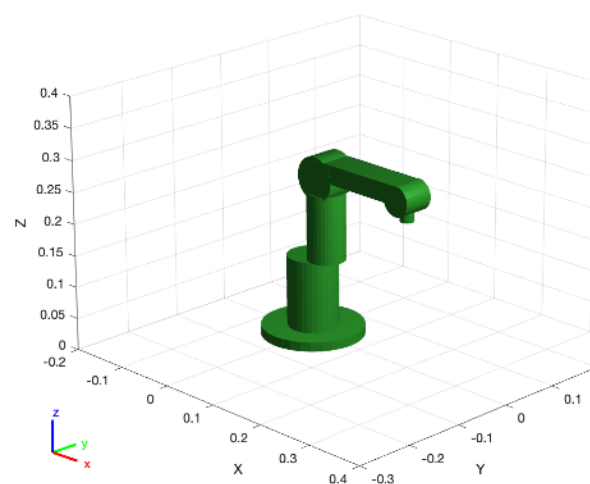
Defined frames

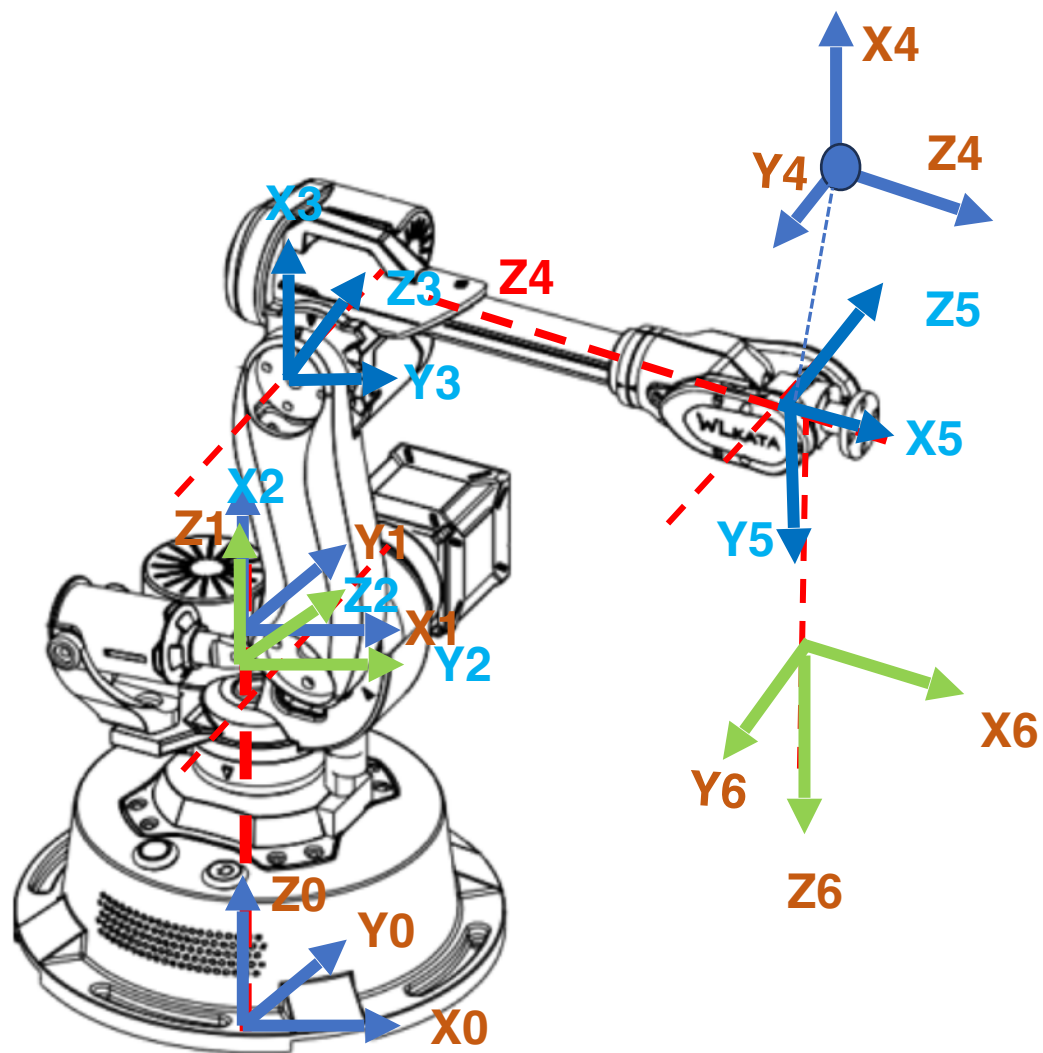


Origin of frames

MDH for CoppeliaSim

frame i	a (i-1)	alpha (i-1)	d (i)	theta (i)
1	0	0	127	0+01
2	29.69	90	0	90+02
3	108	0	0	0+03
4	20	90	168.98	0+04
5	0	-90	0	-90+05
6	0	90	24.29	0+06





MDH for Real Robot

frame i	a (i-1)	alpha (i-1)	d (i)	theta (i)
1	0	0	127	0+01
2	29.69	-90	0	-90+02
3	108	0	0	0+03
4	20	-90	168.98	0+04
5	0	+90	0	+90+05
6	0	-90	24.29	0+06

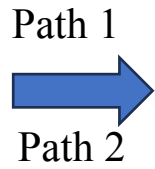
Task 2

Joint Space Control

Task 2: Model

Path Planning

Initial Pose
Intermediate Pose
Final Pose



Quintic Polynomial

$$\begin{cases} \theta(0) = \theta_0 & \dot{\theta}(0) = 0 & \ddot{\theta}(0) = 0 \\ \theta(t_f) = \theta_f & \dot{\theta}(t_f) = 0 & \ddot{\theta}(t_f) = 0 \end{cases}$$



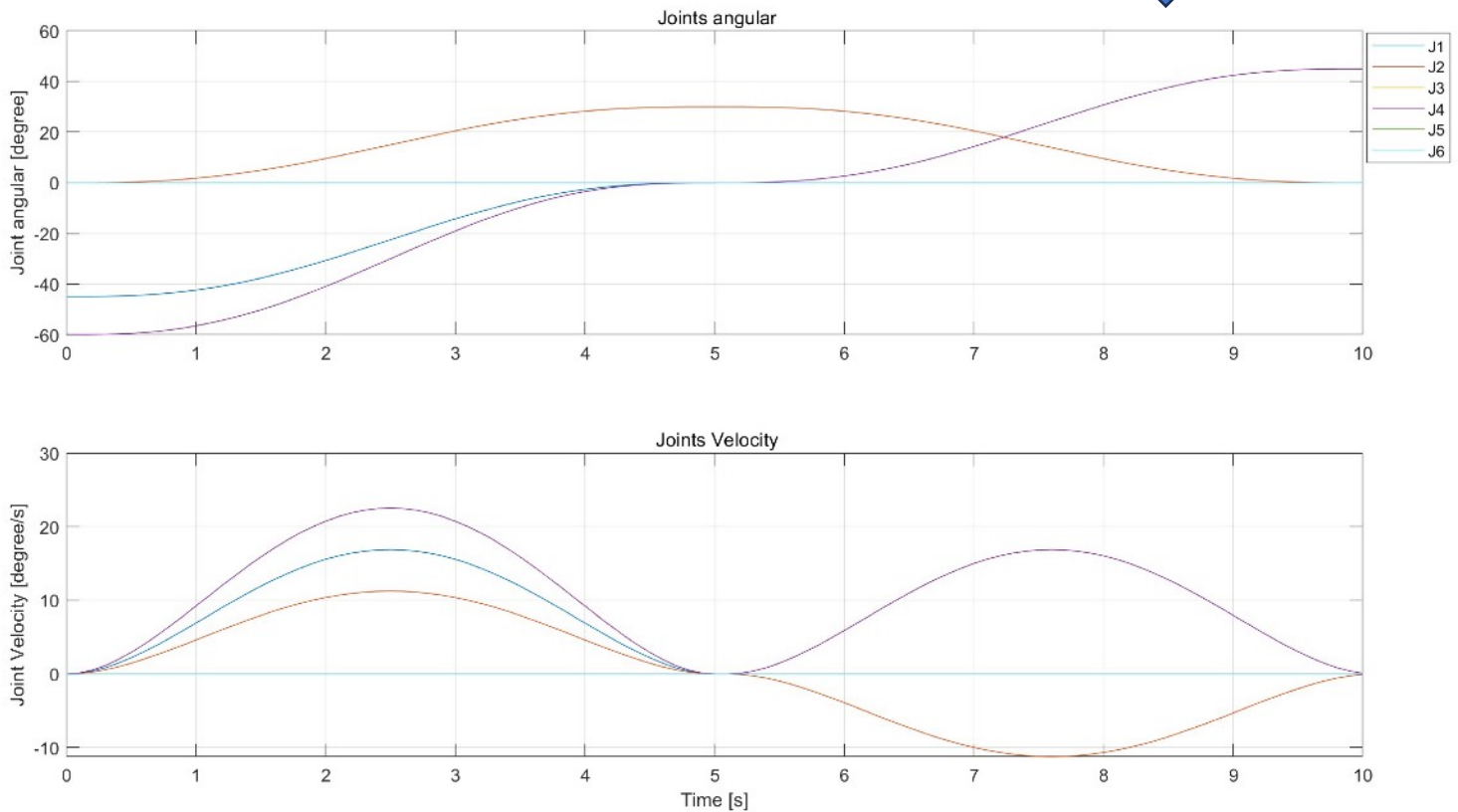
$$\begin{cases} \theta(t) = a_0 + a_1t + a_2t^2 + a_3t^3 + a_4t^4 + a_5t^5 \\ \dot{\theta}(t) = a_1 + 2a_2t + 3a_3t^2 + 4a_4t^3 + 5a_5t^4 \\ \ddot{\theta}(t) = 2a_2 + 6a_3t + 12a_4t^2 + 20a_5t^3 \end{cases}$$

Forward Kinematics



End-Effector Position
In Cartesian Space

Result



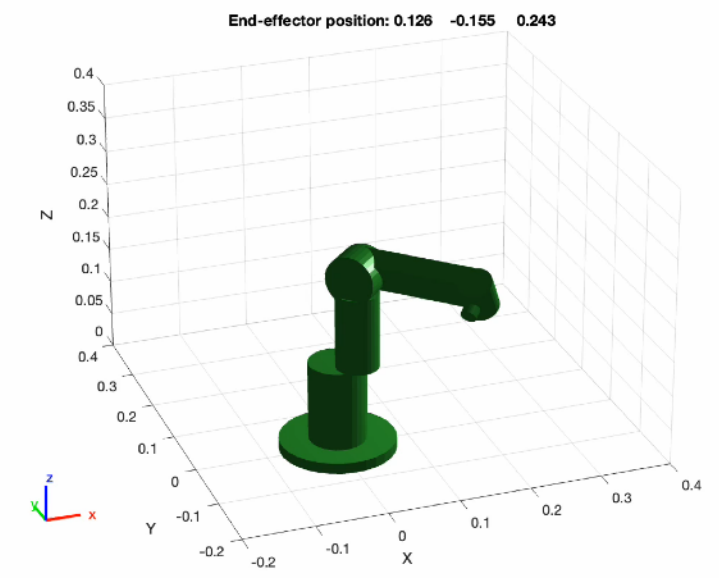
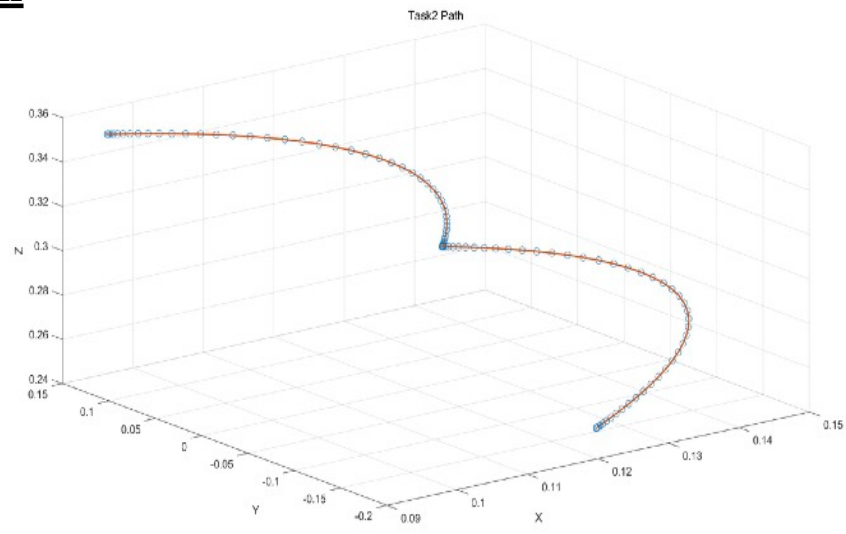
Guarantee Joint Limits

	Angular limit (deg)		Velocity limit (deg/s)
J1	-110	160	85
J2	-35	70	60
J3	-120	60	65
J4	-180	180	200
J5	-200	30	200
J6	-360	360	450

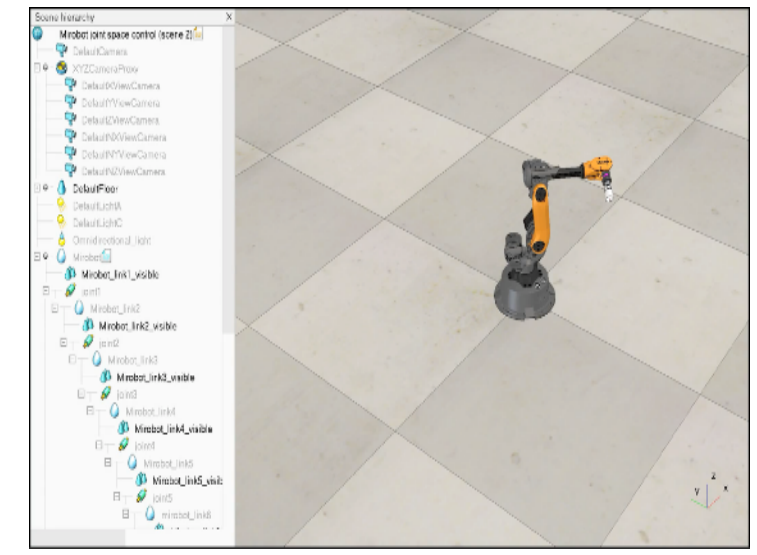
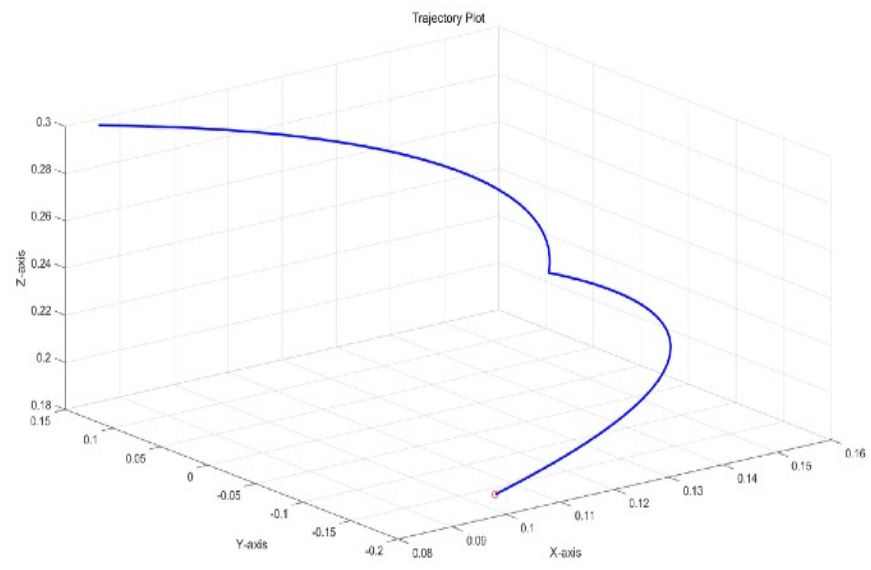
Task 2: Validation

Trajectory Validation

In Matlab



In Coppelia



Task 3

Cartesian Space Control

Task 3

Path Planning

InitialPose
IntermediatePose
FinalPose

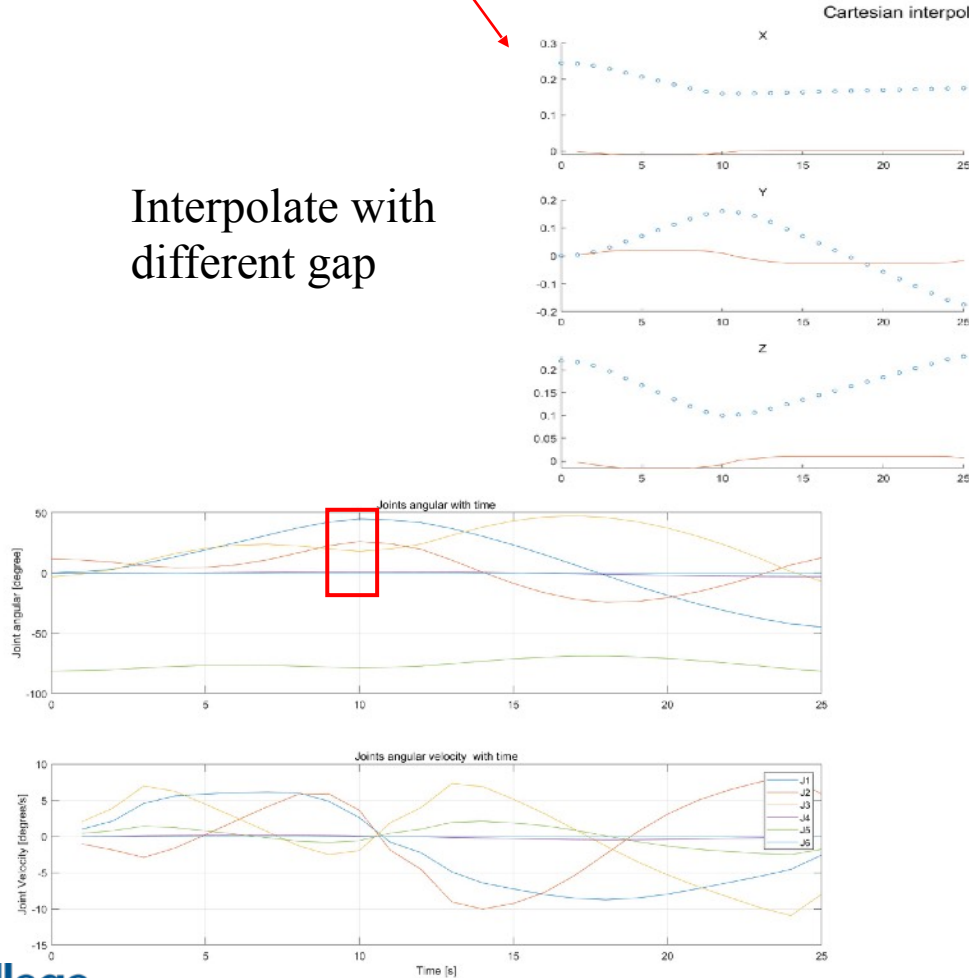
Straight line
Interpolation

Path Planning in
Cartesian Space

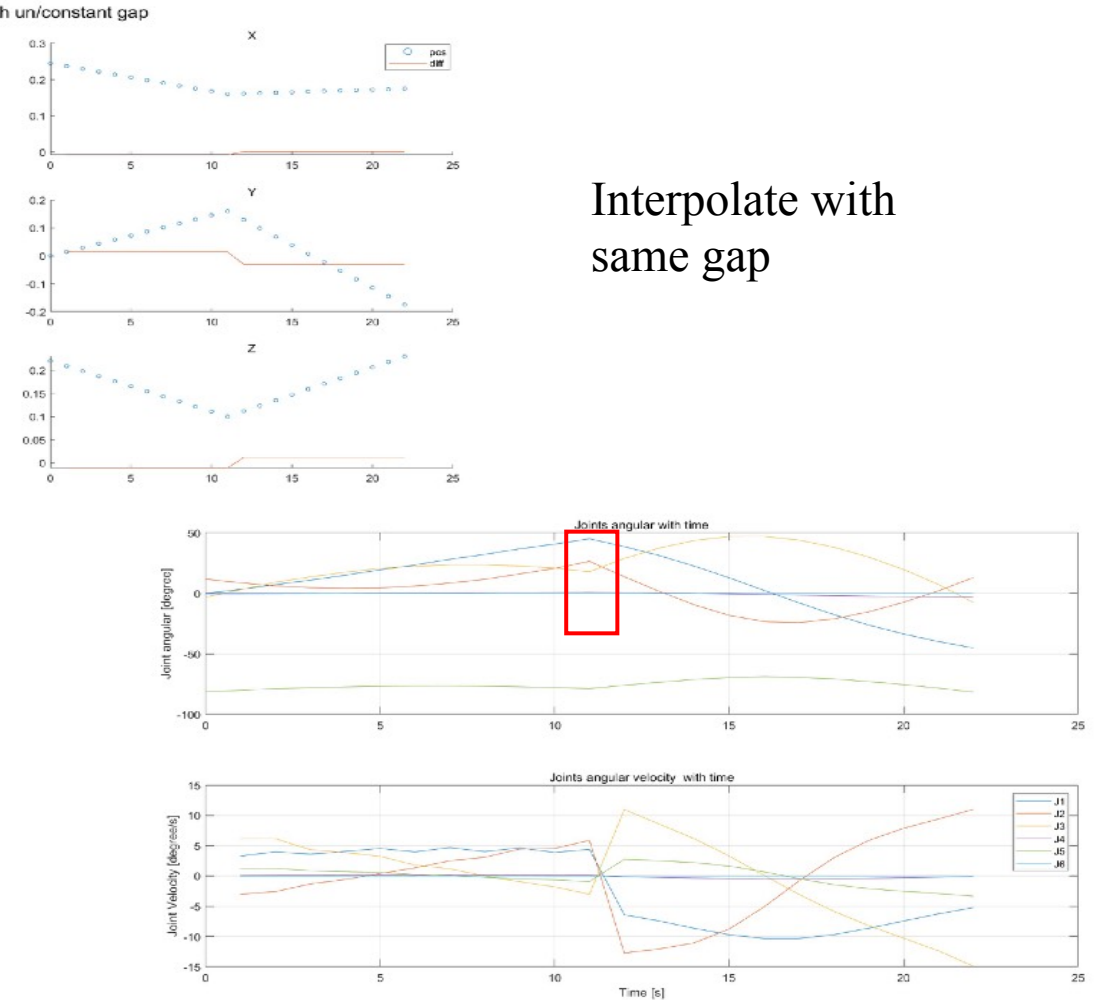
Inverse Kinematics
Jacobian, Joint limits
Newton Iteration

Joints Pose
Joint Movement
Trajectory

Interpolate with
different gap

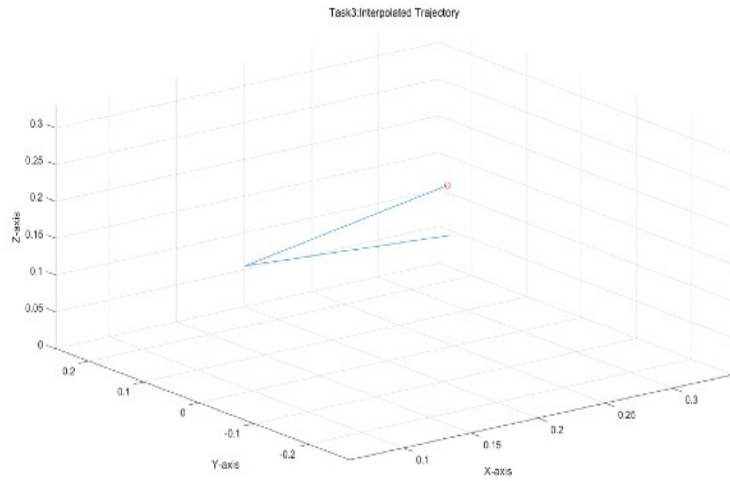


Interpolate with
same gap

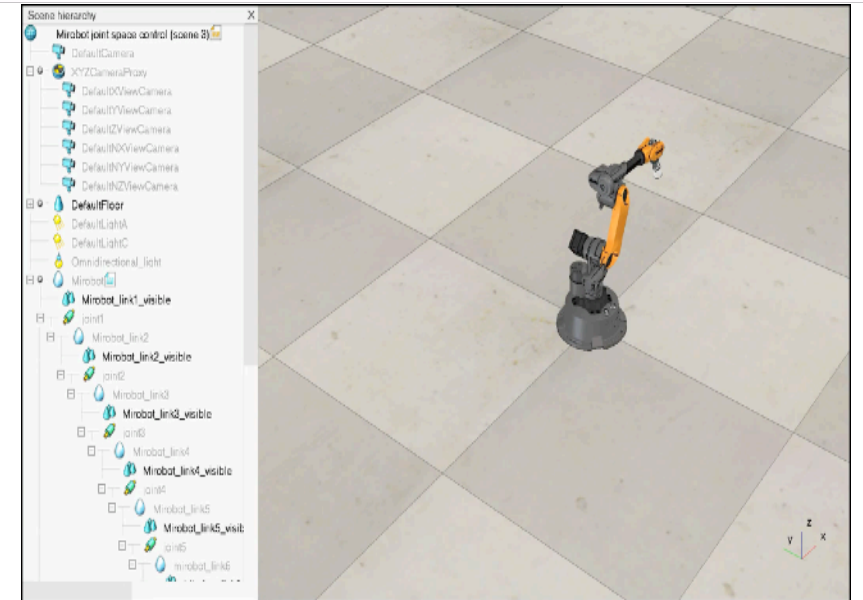
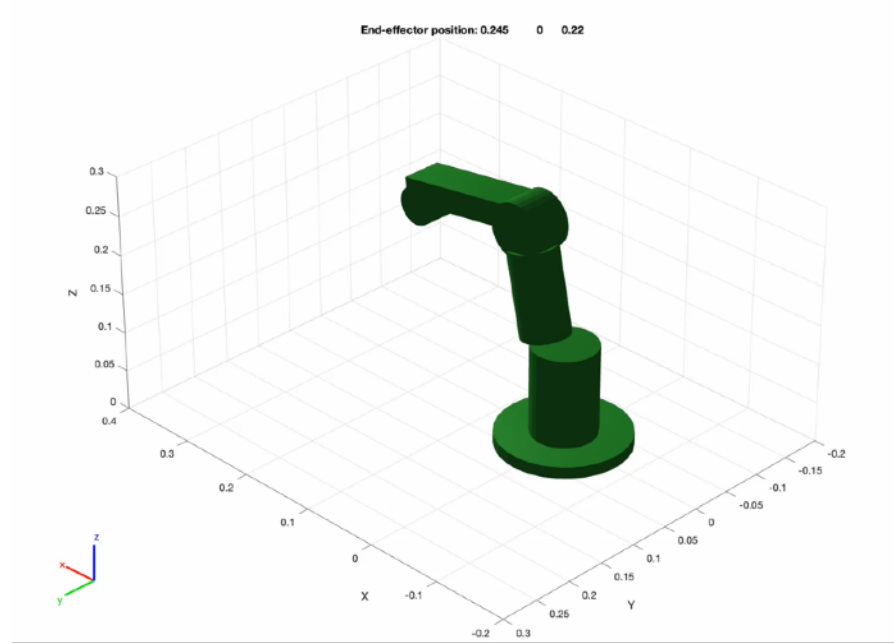
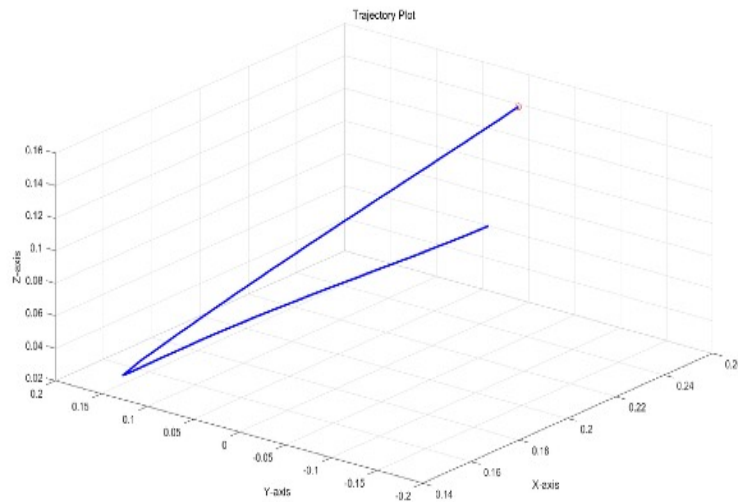


Trajectory Validation

In Matlab



In CoppeliaSim



Difference between Cartesian and Joint space control

Cartesian space control

- Trajectory defined in end effector position
- Easy to visualise trajectory
- Joint motion derived from end effector path through inverse kinematics
- Joint speeds and acceleration can be non-uniform
- Instability near singularities or areas where large changes in joint spaces are required
- Robot independent
- Preferred when control of end effector position is key
e.g. robotic surgery, drawing etc

Joint space control

- Trajectory defined in terms of joint angles/positions
- Not easy to visualize trajectory
- Joint motion controlled hence uniform motion
- The performance is less prone to vibration
- No problem with singularities
- Robot dependent
- Preferred method when space is limited or when carrying out tasks where control over joints is key e.g. obstacle avoidance

Task 4: Robot Pick-and-Place

Three-Finger Soft Gripper



3-Finger Soft
Gripper X 1

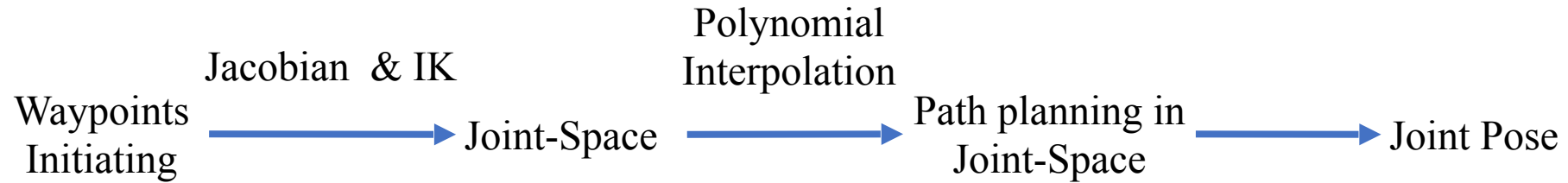


Pneumatic
Box X 1

[1]

Joint-Space Method

Trajectory planning using waypoints



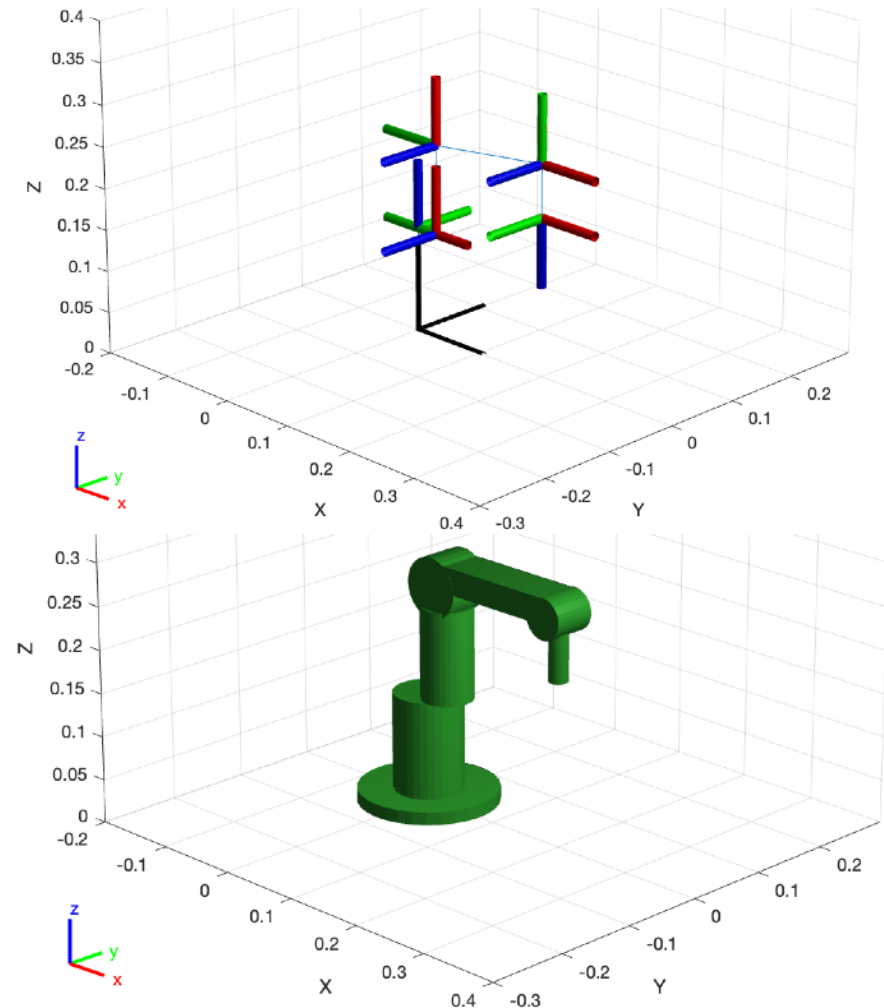
Waypoints	X	Y	Z	Comment
Point 1	0.200	0.150	0.040	Above Cube
Point 2	0.200	0.150	0.025	Pick Cube
Point 3	0.200	0.150	0.070	Up
Point 4	0.000	0.290	0.030	Move
Point 5	0.000	0.290	0.030	Place
Point 6	0.000	0.280	0.070	Up

Challenge 1: Mounting E-E

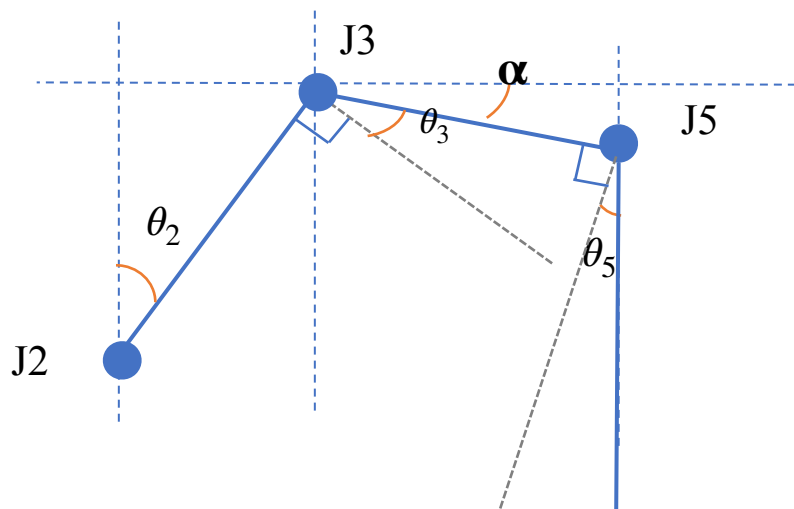
New DH table to
extend link 6 length

frame (i)	a (i-1)	alpha (i-1)	d (i)	theta (i)
1	0	0	127	0+ θ_1
2	29.69	-90	0	-90+ θ_2
3	108	0	0	0+ θ_3
4	20	-90	168.98	0+ θ_4
5	0	+90	0	+90+ θ_5
6	0	-90	24.29+ θ_6	0+ θ_6

New robot model
with end-effector



Challenge 2: Gripper downwards



During Jacobian and IK

$$\theta_5 = -(\theta_2 + \theta_3) = \alpha$$

$$\theta_4 = \theta_6 = 0$$

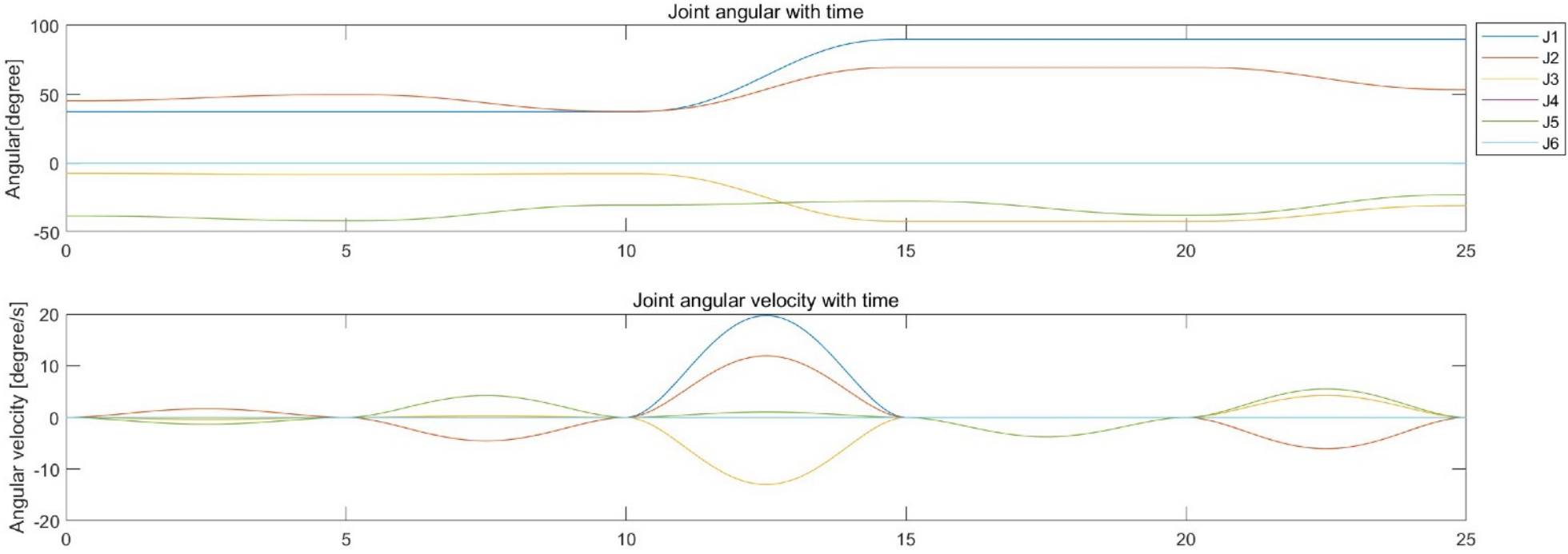
Reach the destination:

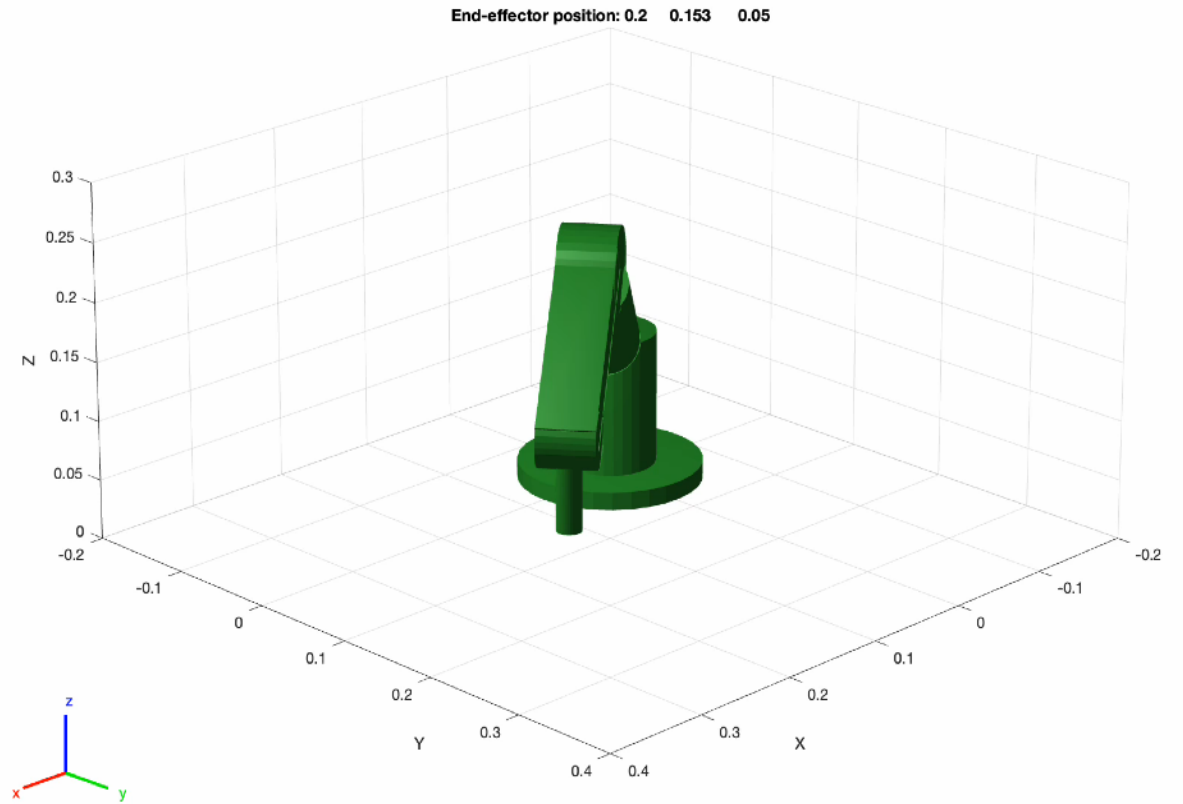
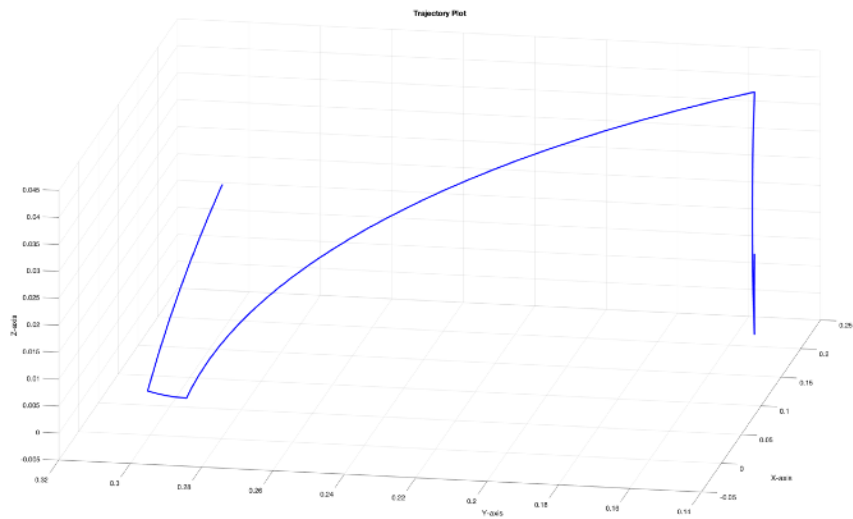
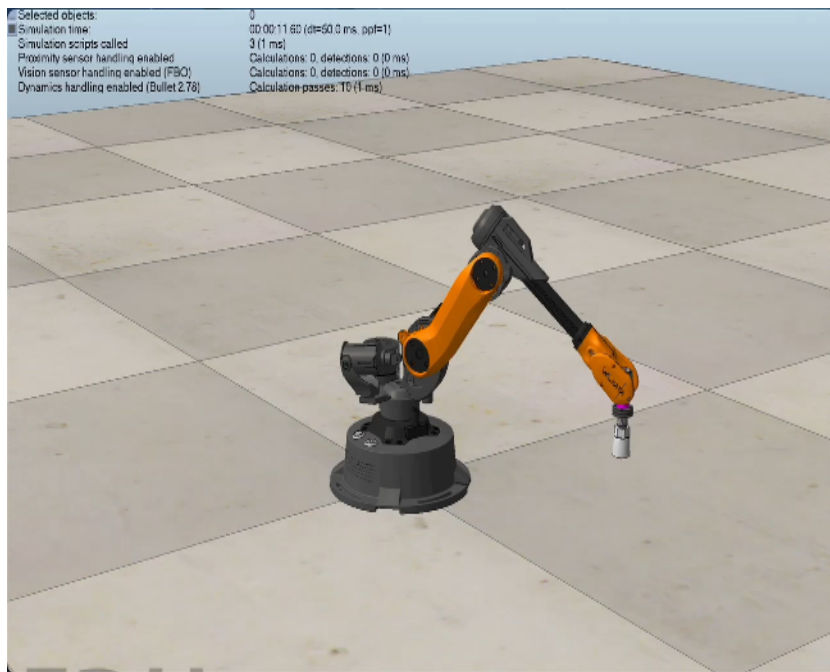
No θ constraints at Point 5

Waypoints	X	Y	Z	Comment
Point 1	0.200	0.150	0.040	Above Cube
Point 2	0.200	0.150	0.025	Pick Cube
Point 3	0.200	0.150	0.070	Up
Point 4	0.000	0.290	0.030	Move
Point 5	0.000	0.290	0.030	Place
Point 6	0.000	0.280	0.070	Up

Simulation Result

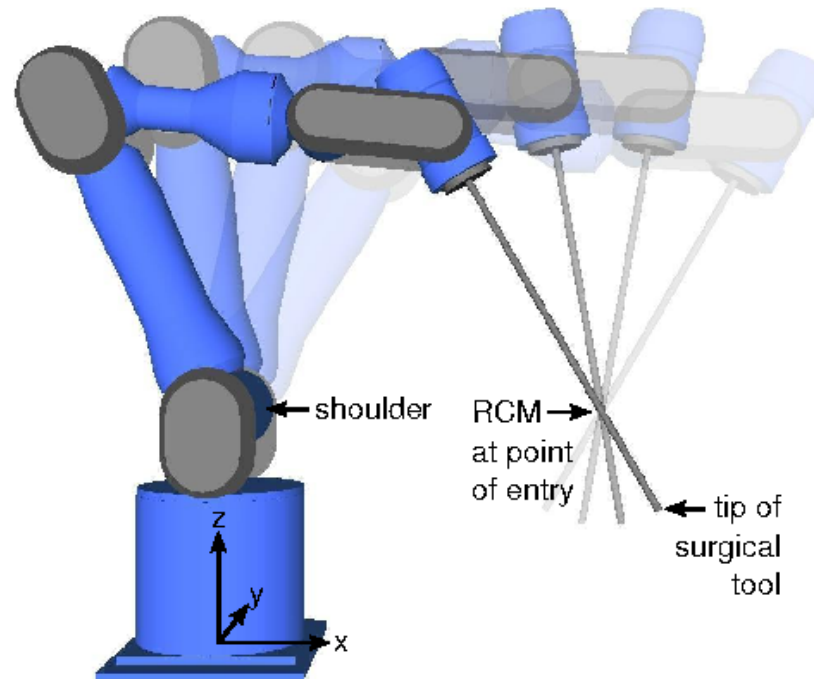
Angular Velocity





Bonus Task

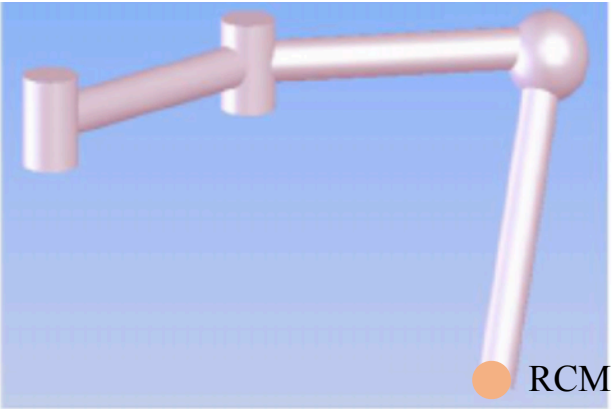
Minimally Invasive Surgery



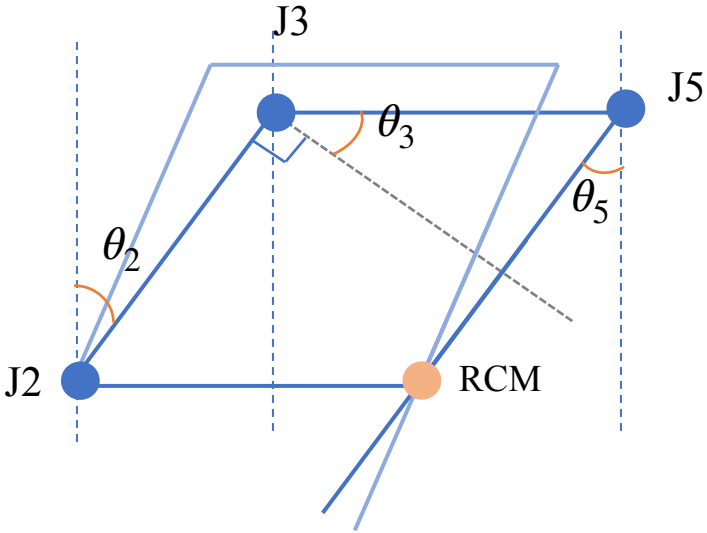
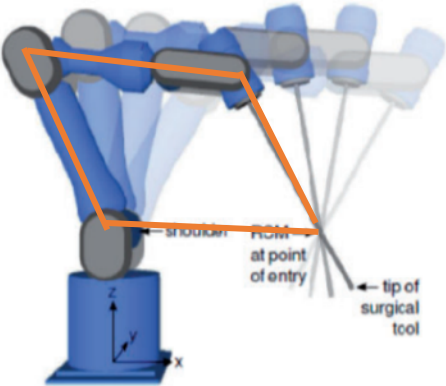
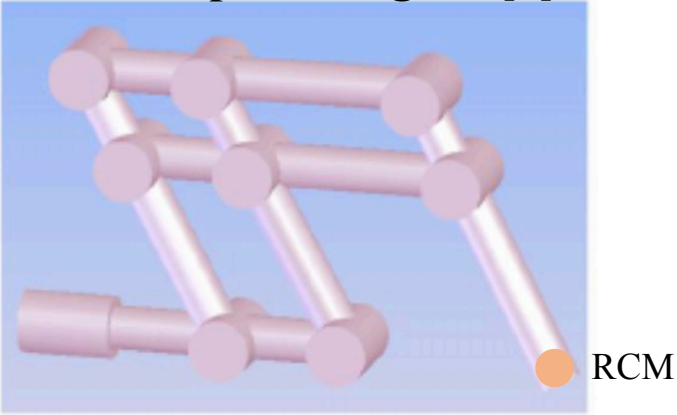
A Robot arm with RCM point illustration [2]

Geometry Solution

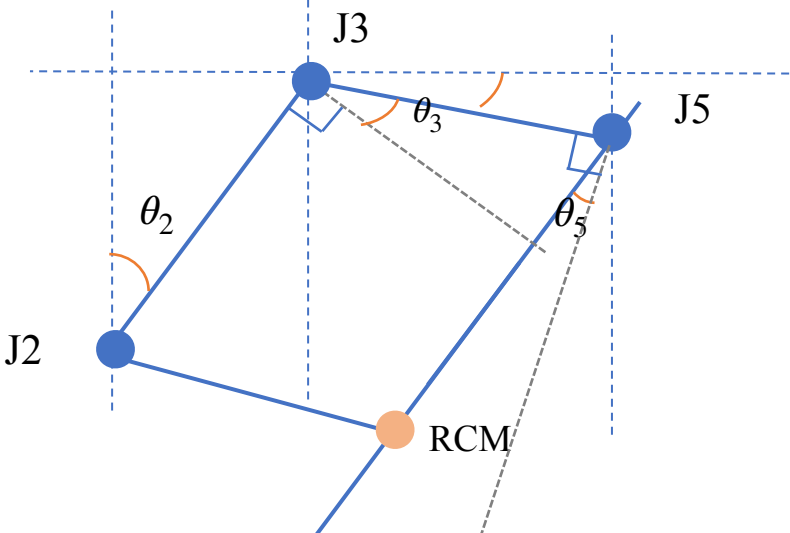
Passive Joint



Double parallelogram[3]



$$\theta_2 = -\theta_3 = \theta_5$$

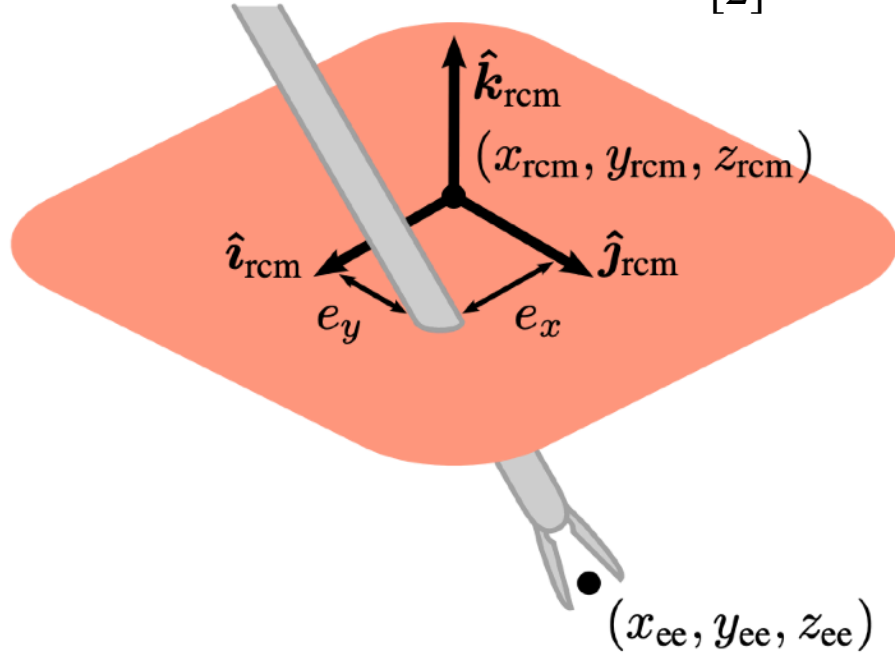


$$\theta_3 = -\theta_5$$

$$\theta_2 = \theta_5 + \alpha$$

Combined with Algebra Solution

[2]



$$J_a = \frac{\partial(x_{ee}, y_{ee}, z_{ee}, e_e, e_y)}{\partial(\theta_1, \theta_2, \theta_3, \theta_4, \theta_5)} \quad \text{Only 3 Variables}$$

Keep End-Effector Horizontal Direction

$$\theta_5 = \theta_2 + \theta_3 - \pi/2$$

Vertical Direction

$$\theta_5 = -(\theta_2 + \theta_3)$$

Reference

- [1] WLKATA Robotics, “WLKATA Robotics Documents” Available at <https://document.wlkata.com/?doc=>
- [2] Locke, R.C., & Patel, R.V. (2007). Optimal Remote Center-of-Motion Location for Robotics-Assisted Minimally-Invasive Surgery. Proceedings 2007 IEEE International Conference on Robotics and Automation, 1900-1905.
- [3] Kim, Sung-Kyun & Shin, Won-Ho & Ko, Seong Young & Kim, Jonathan & Kwon, Dong-Soo. (2008). Design of a compact 5-DOF surgical robot of a spherical mechanism: CURES. IEEE/ASME International Conference on Advanced Intelligent Mechatronics, AIM. 990 - 995. 10.1109/AIM.2008.4601796.

Q & A
Thanks for listening!